





Thesis: Design and control of a robotic mouth

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Contents

1	Intr	oductic	on Control of the Con	1
	1.1	Motiva	ntion	1
	1.2	Goals		2
	1.3	Outlin	e of the thesis	2
2	Lite	rature	Review	3
	2.1	Social	robots	3
	2.2	Why d	o some social robots have a mouth?	4
	2.3	Design	ing a face robot.	4
		2.3.1	Types and material selection	5
		2.3.2	Degrees of freedom: quantity, location and direction	5
		2.3.3	Actuators used for face robots	8
	2.4	Contro	olling a face robot	.2
		2.4.1	Control methods: overview	.2
	2.5	Text to	o robot, general outline	.3
		2.5.1	From sentence or audio up to phoneme segmentation	.4
		2.5.2	From phonemes up to visemes	.4
		2.5.3	From visemes up to mouth shapes	5
		2.5.4	From actuator configurations to fluent speech	.5
3	Des	ign of t	the setup and the mouth 1	7
	3.1	Introd	uction	.7
		3.1.1	Preliminary aspects	.7
	3.2	The te	st setup	8.
	3.3	Contro	olling the setup	8.
		3.3.1	Controlling the servo motors	8.
		3.3.2	Calibration of the servo motors	9
	3.4	Design	ing the mouth	9
		3.4.1	Preliminary aspects	9
		3.4.2	Deformations	0
	3.5	Fixatio	on of the wires on the mouth	2

4	Principle of the method	25
	4.1 Introduction	. 25
	4.2 General outline	
	4.3 From sentence or audio up to phoneme segmentation	
	4.4 From phonemes up to visemes	
	4.5 From visemes up to mouth positions	
	4.6 From mouth positions up to actuator configurations	. 29
5	Calibration Software	37
_	5.1 Introduction	
	5.2 Recognition of the POIs for reference mouths	
	5.3 Recognition of the POIs for the robotic mouth	
	5.4 Mapping servo positions with reference shapes	
6	From actuator configurations to actual speech	41
	6.1 Back to basics	
	6.1.1 Linear interpolation with parabolic blends	
	6.1.2 Clustering phonemes	
	6.1.3 Phoneme importance levels	. 43
7	Tests and results on the setup	47
	7.1 Introduction	. 47
	7.2 Calibration of the test setup	. 47
8	Conclusions	51
•	8.1 Fullfilment of the goals	_
	8.2 Discussion	
	8.3 Future work	
Αŗ	ppendices	53
Α	List of all phonemes for Dutch	55
В	Complete viseme set	57
C	Default sentences	59
D	Servo calibrations	61
		65
	Anatomy of a human face	
Re	eferences	67

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Abstract - English

Human-Robot-Interaction is getting more and more important nowadays. When communication between a robot and human is desired, expressive features may be used in order to enhance the exchange. In order to do so, animatronic heads have been created: Robotic heads that are specifically designed to be expressive or mimic speech.

Several approaches have been used in literature to predict the actuator configurations needed for the desired expressions or mouth shapes. However, these methods are not able to assure a correct result and will most often lead to a final manual tuning of parameters which is time-consuming.

This thesis presents a new approach that can be used to calibrate animatronic heads, omitting the complete knowledge of the mechanical construction and that can be carried out automatically. The new approach has been applied to a robotic mouth that has been designed for this purpose, which gives convincing results.

The approach measures the displacements of some control points on the robotic mouth. The method has been applied in order to mimic Dutch speech.

Keywords: calibration of animatronic head, speech, active feedback, automatic

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Abstract - Nederlands

Mens-robot interactie wordt met de dag belangrijker. Wanneer er communicatie tussen robot en mens gewenst is, kunnen expressieve features worden gebruikt om de qualiteit van de communicatie te verbeteren. Met die doeleinde werden animatronische hoofden ontworpen: Robotische hoofden dat specifiek ontworpen zijn om expressief te zijn en / of spraak na te bootsen.

Er werden in de literatuur verschillende methodes van aanpak getest om vanuit gewenste emotie uitingen of mondvormen de nodige actuator configuraties te voorspellen. Echter zijn deze methodes niet in staat om een correct resultaat te garanderen en is een laatste manuele tuning van de parameters vaak nodig dat veel tijd vraagt.

Deze thesis stelt een nieuwe methode voor dat kan gebruikt worden om animatronische hoofden te calibreren, zonder gebruik te maken van enige kennis over de mechanische constructie en kan volautomatisch worden uitgevoerd. Deze nieuwe methode werd getest op een robotische mond dat voor dit doeleind werd ontworpen en geeft overtuigende resultaten.

De voorgestelde methode gebruikt verplaatsingen van een set controle punten op de robotische mond op een iteratieve manier om zo de nodige actuator configuraties te bepalen. Deze aanpak werd toegepast om met de robotische mond de Nederlandse taal na te bootsen.

Sleutelwoorden: calibreren van animatronisch hoofd, spraak, feedback, automatisch

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Abstrait - Français

De nos jours, l'interaction humain-robot devient de plus en plus importante. Quand une communication entre un robot et un humain est désirée, des expressions caractéristiques peuvent être utilisées pour améliorer l'échange. Pour ce faire, des têtes animatroniques ont été créées : des têtes robotisées qui sont spécialement conçues pour être expressives ou imiter la parole.

Plusieurs approches ont été suivies dans la litérature pour prédire les configurations des actionneurs nécessaires à l'expression désirée ou la forme de la bouche. Ceci dit, ces méthodes ne sont pas capables d'assurer un résultat correct et requièrent souvent un ajustement manuel final des paramètres ce qui prend du temps.

Ce mémoire présente une nouvelle approche qui peut être utilisée pour calibrer les têtes animatroniques, en omettant la connaissance exhaustive de la construction mécanique, et qui peut être gérée automatiquement. Cette nouvelle approche a été appliquée à une bouche robotisée conçue pour cet usage et donne des résultats convaincants.

L'approche mesure les déplacements de certains points de contrôle sur la bouche robotisée de manière iterative pour determiner la configuration des actionneurs. La méthode a été appliquée afin d'imiter le language flamand.

Mots clés: calibration de tête animatronique, parole, feedback, automatique

List of Figures

2.1	Several examples of face robots	6
2.2	Some commonly used AUs and their interpretations	7
2.3	A representation of anger in the parametrised facial muscle model of Waters	8
2.4	A servo and its internal structure	ç
2.5	The routing of SMAs in an animatronic baby head, using pulleys	10
2.6	The McKibben actuator	10
2.7	The internal structure of the robot Saya using McKibben muscles	11
2.8	An ACDIS actuator, a pneumatic actuator	11
2.9	A structural graph showing the layout of the applied methods in literature	13
2.10	The different steps up to the actuation of the mouth	13
2.11	A graphical representation of a segmented audio file	14
3.1	The test setup that has been designed during this thesis	18
3.2	The distribution board for feeding the servos	19
3.3	The mouth seen from different angles	20
3.4	Different planar structures that were tested for deformations	21
3.5	The two possible ways to stretch a hexagonal structure	22
3.6	The open mouth with a hexagon internal structure, seen from different angles	22
3.7	The pose of the wires actuating the flexible mouth	23
4.1	A flowchart showing the layout of the applied methods in literature	25
4.2	A flowchart showing the layout of the new proposed approach	26
4.3	The different steps up to the actuation of the mouth	26
4.4	A subset of visemes	28
4.5	The POIs on a dummy mouth along with the definition of a reference frame	29
4.6	The feedback loop of the implemented algorithm	31
4.7	The oscillations appearing due to coupling of actuators	34
4.8	Variable gain techniques compared to fixed gain control	34
4.9	Near convergence using a linear varying gain control strategy	35
4.10	The absence of coupled oscillatory phenomena with a variable gain strategy .	36
5.1	A subset of reference mouth shapes	37
5.2	The recognition of mouth shapes	38
5.3	The interface of the calibration script	39

6.1	A graphical representation of a segmented audio file	42
6.2	The similar visual representations of phonemes p and b	43
6.3	The influence of hiding invisible phonemes in a segmentation file	45
7.1	Comparison of calibration results with reference pictures, part 1	48
7.2	Comparison of calibration results with reference pictures, part 2	48
7.3	The calibration results, graphically represented	49
A.1	A reference list of all the phonemes for the Dutch language	56
B.1	A reference list of all the visemes used to represent the Dutch language	58
E.1	The major muscles having a direct effect on lip deformations	66

List of Tables

	The 5-point scale intensity coding of FACS	
4.1	The time needed to create a database in function of the number of servos .	32
	The clustering of phonemes that has been used in this thesis	
C.1	Standard sentences in Dutch along with their translation in English	60
	Calibration results of each servo, part 1	

Abbreviations

DOF Degrees of Freedom

FACS Facial Action Coding System

AU Action Unit

SMA Shape Memory Alloy

PWM Pulse-Width Modulated

POI Point Of Interest

PTD Protected

INV Invisible

MID Normal

Chapter 1

Introduction

Animatronic¹ heads have amazed people for a long time, as these are able to express emotions or even mimic speech. Behind this simple looking face, resides a considerable amount of know-how. Years of research have given us the ability to build realistic looking heads that closely resemble humans. Such animatronic constructions are also called humanoids.

One of the main difficulties in expressing emotions or mimicing speech with an animatronic head, is closing the gap between the desired expression / mouth shape and the therefore needed actuator configuration.

1.1 Motivation

Several solutions exist, but lack of robustness. All methods but the trial-and-error approach are not able to assure that the predicted actuator configurations will give the desired emotions or correct mouth shapes, as these don't use the real animatronic head, but a model of it. This results in a highly probable final need to further tune the configuration settings of the actuators, thus bringing us back to trial-and-error solutions.

Convincing results require skilled people, often animators, in order to actuate the head. Depending on the number of degrees of freedom (DOFs), this can take time. Next to that, a small change in the mechanical configuration might cause a need to partially or completely recalibrate the head.

The trial-and-error solution works for a small set of emotions, but gives a problem when tackling speech mimicing, as many mouth shapes are necessary in order to properly mimic speech. This is a problem.

¹Animatronic is a portmanteau for animate and electronics.

1.2 Goals

The goal of this thesis is to present a new approach that could be used to calibrate robotic mouths in order to properly mimic speech.

In order to validate this concept, a test setup has to be designed, consisting of a robotic mouth, which will be calibrated with the new approach.

The quality of the approach will be assested by the use of a lip-synchronisation module, which will allow to mimic speech.

The new approach should be able to:

- 1. Calibrate the robotic mouth by omitting the complete knowledge of the robotic head;
- 2. Do this fully automatically;
- 3. allow an objective evaluation about the configuration quality of the DOFs that are implemented in the mouth.

1.3 Outline of the thesis

In chapter 2, a literature review will be given. First social robots will be introduced and it will be shown why most of them need a mouth. Practical design considerations will be given with a focus on how DOFs should be chosen as well as how these have been implemented in the literature.

Next, the methods for controlling the face robots will be shown shown as well as what the required steps are in order to mimic speech.

Then, in chapter 3 a complete setup is proposed to study a new approach for calibrating face robots.

In chapter 4, the principle used to fulfill the defined goals is explained in detail along with the different steps needed to transform a sentence or audio to a sequence of calibrated mouth shapes.

Next, chapter 5 presents the software that has been designed for calibrating the robotic mouth. Then, chapter 6 discusses the steps that have to be taken in order to go from a sequence of mouth shapes towards fluent speech. Concepts as the *clustering of phonemes* and *phoneme importance levels* are presented.

Chapter 7 shows the results of the calibration method for some phonemes and discusses the results.

Finally, Chapter 8 summarizes and evaluates the results of this thesis along with possible future work.

Chapter 2

Literature Review

2.1 Social robots

What is a social robot? Bartneck and Forlizzi gave the following definition of a social robot (Bartneck & Forlizzi, 2004):

A social robot is an autonomous or semi-autonomous robot that interacts and communicates with humans by following the behavioral norms expected by the people with whom the robot is intended to interact.

Social robots exist in many forms and the application fields are numerous. For example, social robots may be used in

- Service applications
- Education
- Therapy

Social robots can be used to serve as durative assistant. There is a significant proportion of elderly, which is increasing year by year (Lutz et al., 2008), while the social care facilities are already insufficient at this moment. In order to face these problems, social robots are proposed as a solution which may prolong the autonomy of elderly, thus further delaying a move to care facilities. In such an application, the social feature of the robot is a necessity, in order to improve the collaboration with the user with great efficacy (Wilkes et al., 1998). Social robots can also be used in order to improve education, for example, as guide in a museum. It has been shown that the use of a social robot has a positive impact on the education quality (Nourbakhsh et al., 1999).

On the other hand, social robots can be used in therapy. They can be used in therapeutic programs for autistic children. Probo is an example of such a social robot (as seen in Figure 2.1b). The robots are used to interact with autistic children, to teach skills, play with them and to elicit certain desired behaviours from them (Cabibihan et al., 2013; Werry et al., 2001).

2.2 Why do some social robots have a mouth?

Communication has always been a very important aspect when collaboration is necessary. When communication between a robot and a human is important, facial features are added to the robot. This is done in order to increase the understandability of the robot, as well as his believability (Breazeal, 2000), as believability is influenced by the degree of antropomorphism (Nowak & Rauh, 2008).

Besides communication, the ability to show emotions is a key aspect that is needed to assure the believablity of a social agent (Bates, 1994), such as a social robot. Also, research has shown that communicating about emotional states is done for 55% using expression (Mehrabian, 1971). It is for those reasons that social robots are equipped with expressive features to increase its humanness and believability. Several features contribute more than others and it has been found that a pair of eyes and a mouth contribute the most to the perception of humanness of a social robot (DiSalvo et al., 2002).

However, it is important to realize that seeking humanness in so-called humanoids has its limits. When a humanoid closely resembles the human, any deviation from a normal behavior will be noticed, entailing an immediate repulsion towards the humanoid. This effect is known as the uncanny valley effect (Mori et al., 2012).

In order to further increase the communication quality, new mediums may be sought in order to communicate. For example, mimicing speech can be used to communicate between robot and human as it is the default medium people use to communicate.

It has been shown that speech intelligibility is drastically increased when supplementary visual observation of the speaker's facial and lip movements is available (Sumby & Pollack, 1954). On the other hand, visual information of the lip affects the perception of the audio information. An example of such influence is the McGurk effect (McGurk & MacDonald, 1976). The McGurk effect shows that visual information changes the perception of the audio information as the receiver treats both audio and visual information together. This shows that the use of a mouth to increase the intelligibility of speech of a social robot should be implemented and controlled as such that is has a beneficial influence on the communication quality.

2.3 Designing a face robot.

When designing an antropomorphic head, a lot of important steps must be taken. The content of these steps will be a result of the following fundamental questions:

- What will the head look like?
- What kind of materials will be used?
- How many degrees of freedom will be implemented?

- Where are those degrees of freedom located and in which direction do these act?
- How do I actuate those degrees of freedom?

2.3.1 Types and material selection

Face robots can be split in to two main groups: one having rigid face components and the other having flexible facial components. Examples are shown in Figure 2.1 The material choice for the face of a rigid face robot is entirely based on material constraints and aesthetics. On the other hand, designing a face robot with flexible parts adds complexity, as deformations have to be taken into account. A combination of the two is also possible as is the animatronic head Flobi, shown in Figure 2.1a.

When a humanoid face is designed, higher complexities are involved, as deformations are overall present and are used in order to express emotions. Materials that are used should mimic human skin. Being elastic is thus a main requirement. An appropriate material is rubber, which is used in almost all humanoid heads.

A new material that has recently been developed is called Frubber, which is a patented deformable material developed at Hanson Robotics (Hanson Robotics, n.d.). Frubber is a contraction of flesh and rubber, standing for its ability to mimic human flesh more accurately than any other known technology, using 1/20th of the power that other materials need. An example of a realistic face robot built with Frubber is Jules, shown in Figure 2.1d.

2.3.2 Degrees of freedom: quantity, location and direction

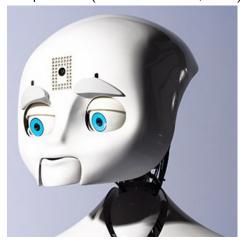
The number of DOFs will depend on the level of realism that is required. The position and direction of those DOFs will have to be chosen as such that the facial expression or mouth shapes can be formed. One can make his choice based on the facial action coding system (Friesen & Ekman, 1978).



components. (Lütkebohle et al., 2010)



(a) Flobi, which has rigid and flexible facial (b) The social robot Probo, (Saldien et al., 2010), which is covered in fur.



(c) The robot Nexi, MIT, (Personal Robots Group, 2015), with rigid facial components.



(d) Jules, Hanson Robotics, (Jaeckel et al., 2008), has a skin made of Frubber.

Figure 2.1: Several examples of face robots.

The Facial Action Coding System (FACS) is an anatomically based system for measuring all visually discernible facial movements, using 44 action units (AUs). Each AU consists of a set of muscles, involved in each action. There is not a one-on-one relationship between muscle groups and AUs, as several muscles have various visual effects. FACS even allows a coding of the intensity of each facial action on a 5-point intensity scale, 2.1

Table 2.1: The 5-point scale intensity coding of FACS

A B C D E trace slight marked severe maximum

The FACS system has been used to describe the 6 basic emotions of Ekman (Eckman, 1972), being: anger, sadness, happiness, disgust, surprise and fear (Matsumoto & Ekman, 2008). The descriptions are shown in Table 2.2.

Locating the AUs needed for the emotive expressions as well as their line of action, proposes locations and directions that can be used to design a humanoid head. Besides that, the system shows which AUs are used for each emotion. The FACS system has been used to design animatronic heads in a lot of research projects (Weiguo et al., 2004; T. Hashimoto et al., 2004, 2006; Lin & Huang, 2009; Lin, Huang, & Cheng, 2011; Thayer, 2011; Lin et al., 2012, 2013; Loza et al., 2013; Baldrighi et al., 2014; Asheber et al., 2015).

Some commonly used AUs and their interpretations are shown in Figure 2.2.

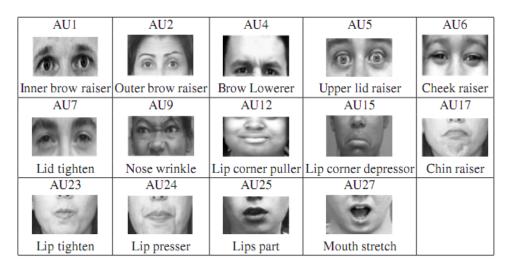


Figure 2.2: Some commonly used AUs and their interpretations (Zhang, L, 2008).

Exceptionally (Lin, Cheng, et al., 2011) the design of such a head has been done using the parametrised facial muscle model of Waters (Waters, 1987). In Figure 2.3, the muscle model for *anger* is shown. The 6 basic emotions of Ekman have also been developed in this model, using FACS to validate the results.

Table 2.2: Action Units associated with emotion, (Matsumoto & Ekman, 2008)

Facial Expression	AUs
Anger	4,5 and/or 7, 22, 23, 24
Disgust	9 and/or 10,25 or 26
Fear	1,2,4,5,7,20,25 or 26
Happiness	6,12
Sadness	1,4,15,17
Surprise	1,2,5,25 or 26

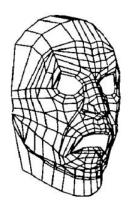


Figure 2.3: A representation of anger in the parametrised facial muscle model of Waters (Waters, 1987).

2.3.3 Actuators used for face robots

Several types of actuators are commonly used in face robots. They can be grouped in three categories:

- 1. Servos
- 2. Shape Memory Alloy (SMA) actuators
- 3. Pneumatic actuators

This is a non-exhaustive list only recalling the most frequently used actuators for face robots.

Servo motors

An example of a servo motor is shown in Figure 2.4. Servos and motors are most often used due to their simplicity in control and modular aspect, as they can be fixed anywhere needed and do not take much space (Weiguo et al., 2004; T. Hashimoto et al., 2006; Oh et al., 2006; Jaeckel et al., 2008; Allison, 2009; Lin & Huang, 2009; Lütkebohle et al., 2010; Lin, Cheng, et al., 2011; Lin et al., 2013; Baldrighi et al., 2014). Servos are a mature technology, they have been used in many applications, ranging from animatronics to hobbyist Radio-Controlled

vehicles. There are no technical difficulties added, as the system is controlled internally. One of the disadvantages is that servos can be noisy and may have problems regarding heat dissipation when used for a long amount of time.

A servo consists of several components. It has a DC motor inside, a gear transmission, a circuit board and a potentiometer. The potentiometer is connected to the output shaft after the gearing transmission. It is used as an encoder which reads the angular position of the shaft. The gear transmission is used to put down output speed, while increasing output torque. The circuit board of the servo compares the potentiometer's measurement to the reference input signal, which is a Pulse-Width Modulated (PWM) signal. Changing the duty cycle of the input PWM signal will change the position of the servo. As a servo uses a PWM signal to control its angular position, there is a minimal reaction time which cannot be reduced. The PWM signal has a period of 20ms, wherein the servo motor is evaluating the duty cycle, in order to regulate its angular position.

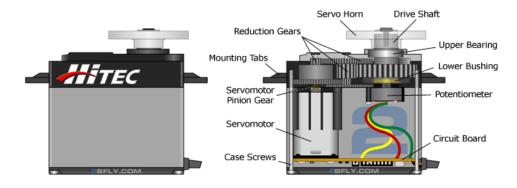


Figure 2.4: A servo and its internal structure (2BrothersHobby, 2016).

SMA actuators

An SMA actuator is a wire made of a special alloy, that change length when heat is provided. As the actuator is conductive, the heat is provided by applying a current through the alloy. Using SMA actuators brings several complications with it, as these have a certain latence in their response. Also, in order to get a certain displacement, a certain length of SMA is needed. For example, when an SMA actuator that contracts 4% is used to move 1 cm, a total wire length of 25 cm is necessary.

As the wires are conductive, it is important that SMAs do not touch each other, as the behavior of the mechanism will be corrupted. Another important problem is the heat that is dissipating from the wire, which should be evacuated at all cost from the head model, for safety reasons and proper functioning. A depiction of the routing of SMA actuation is shown in Figure 2.5. The use of pulleys allows to compact the total SMA length. Despite their complexity to use, SMAs have been used in the past (Hara et al., 2001; Tadesse et al., 2011). Also, controlling the contraction of such an SMA is difficult. As it uses heat, its behavior after the appliance of heat is completely dependent on the heat conductivity of the SMA

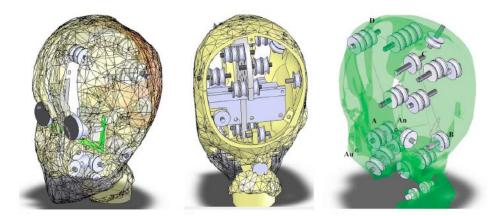


Figure 2.5: The routing of SMAs in an animatronic baby head, using pulleys (Tadesse et al., 2011).

itself, limiting the speed at which it can be actioned. SMAs are often cooled with a built-in fan to limit this problem.

Pneumatic actuators

Pneumatic actuators are also used regarding the actuation of animatronic heads, under several forms. The most common use of pneumatic actuation uses McKibben actuators. A McKibben actuator is shown in Figure 2.6.

McKibben actuators consist of an internal bladder surrounded by a braided mesh shell.

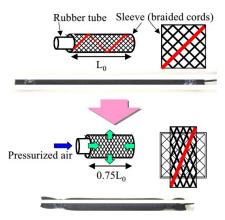


Figure 2.6: The McKibben muscle, a pneumatic actuator that shortens when pressure is applied. (T. Hashimoto et al., 2006)

On one side, there is a canal leading to a controlled pressure source. The other side of the bladder is closed. When pressure is applied, the actuator shrinks in length and thickens in width, thus acting as a muscle (as shown in Figure 2.6). The face robot Saya, whose internal

structure is shown in Figure 2.7, uses McKibben actuators for facial expressions. The black components are the McKibben actuators.

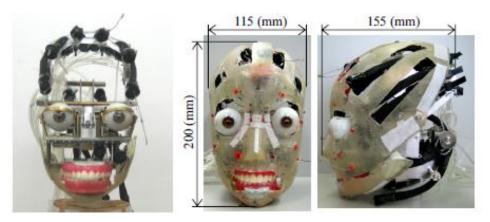


Figure 2.7: The internal structure of Saya (T. Hashimoto et al., 2006). The black components are McKibben muscles, used to pull strings, attached to the skin of Saya.

An other example of pneumatic actuation is an ACDIS (Hara & Endo, 2000), which stands for ACtuator including DIStance measurement. Such an ACDIS is shown in Figure 2.8. It is a pneumatic actuator which is equipped with a double-action piston, along with an LED and a photo transistor. The LED and photo transistor are used to control the position of the double-action piston, which is moved using a source of pressurised air. It is not often used. The main problem of using such an apparatus is that the dynamic behavior of the

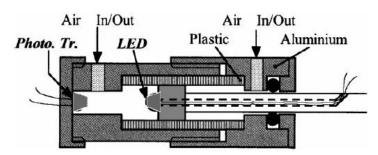


Figure 2.8: An ACDIS actuator, as used in (Hara & Endo, 2000).

actuator is dependent on the compressibility of air, which plays a significant role. Also, as with all pneumatic actuators, a constant pressure source is needed in order to actuate the head, which cannot be a built-in feature. A pressure source is not always available. For solving this problem, a compressor may be used. The main disadvantage is that it is a voluminous component, which makes a lot of noise when pressurizing its air reservoir.

Overview actuation methods

Regarding the previous listing of actuators, one can see that using servos has many advantages regarding control techniques and modularity. Using pneumatics entails possible leakage

problems which are not easy to trace back. SMA actuators have an intrincic routing problem due to their inherent working principle. On the other hand, servos are compact, are easily replacable and cheap depending on their quality and they have a relatively long lifecycle, compared to SMAs. The only disadvantage of using servos is the noise they can generate during movement.

2.4 Controlling a face robot

One of the main difficulties in expressing emotions or mimicing speech with an animatronic head, is closing the gap between the desired expression / mouth shape and the therefore needed actuator configuration.

Solutions for this issue do exist. For example, actuator configurations can be predicted by using a Finite Element Method (FEM) model where emotions are experimentally reproduced and deformation are evaluated (Weiguo et al., 2004; Tadesse et al., 2011; Bickel et al., 2012; Baldrighi et al., 2014). The quality of this result greatly depends on the quality of the model and how complete the head was modeled. This can easily be done when the head is built out of rigid parts. However, modelling a humanoid head having a deformable skin is not straightforward, as it is not simple to model a highly elastic, non-linear material.

An other solution exists in experimentally determining which configuration is needed for each emotion or mouth shape (Hara & Endo, 2000; Jaeckel et al., 2008; Kobayashi et al., 2002; Hara et al., 2001). This approach is not optimal, as this is manually done. Realistic humanoid heads have a lot of actuators (as the humanoid Albert HUBO, (Oh et al., 2006), which has 31 degrees of freedom in his head), which shows that this solution takes time and is tideous.

A different approach consists in measuring muscle activities on a human face expressing several emotions and projecting these on the working range of the humanoid's head (M. Hashimoto et al., 2006). In this research, muscle activities are measured for each facial muscle group that is implemented in the face robot. This is done when the subject contracts each facial muscle as best as possible. The same measurements are repeated when the 6 basic emotions are expressed. Then, the maximal displacement on the subject's face is measured for the different muscles. Next, the wire tension and displacements of the robotic head are measured in order to define a concept of stiffness. The muscle activities for each expression are then first translated towards displacements. Finally, those displacements are converted to wire tensions thanks to the previously defined stiffness. This approach is valid in this case as the robotic head is a replica of the subject itself.

2.4.1 Control methods: overview

It is clear that there does not exist a universal solution to this problem except the trialand-error approach. The control methods that have been defined in this section, can all be

¹A humanoid = An antropomorphic robot

represented with the same structural layout, as shown in Figure 2.9 as they all use the same basic principle. A method is used to provide a prediction of the actuator configuration needed for each emotion or mouth shape. This prediction is then applied and eventually, the results are manually modified in an iterative fashion to get convincing results. Before the iterative step, the real head is never used.

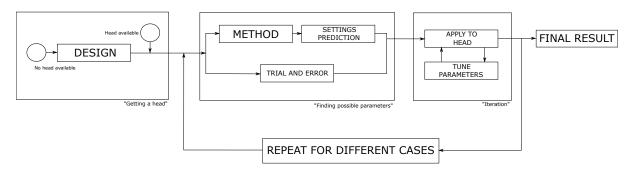


Figure 2.9: A structural graph showing the layout of the applied methods in literature

2.5 Text to robot, general outline

In order to make a face robot mimic speech, several steps need to be taken. These steps are shown in Figure 2.10.

$$\left\{ \begin{array}{l} \mathsf{SENTENCE} \\ \mathsf{AUDIO} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathsf{PHONEME} \\ \mathsf{SEGMENTATION} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathsf{VISEME} \\ \mathsf{SEGMENTATION} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathsf{MOUTH} \\ \mathsf{POSITIONS} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathsf{MOUTH} \\ \mathsf{POSITIONS} \end{array} \right\}$$

Figure 2.10: The different steps up to the actuation of the mouth

The different forms of data in the process are:

- an audio file, a sentence, or any equivalent information form;
- a list of phonemes² and an associated segmentation file containing timings;
- a list of visemes³ and an associated segmentation file containing timings;
- actuation parameters that will shape the mouth into the desired form;
- a final result matching the desired sentence in a fluent way.

Between every information type, there is a conversion that has to be done.

²A phoneme is every basic unit of speech. A language can be represented with a sequence of phonemes. Examples are p, b, m for the Dutch language.

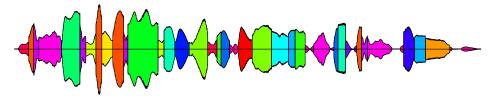
³A viseme is the visual equivalent of a phoneme.

2.5.1 From sentence or audio up to phoneme segmentation

The conversion starts with the translation of a sentence or an audio file to a phoneme segmentation file. A phoneme segmentation file is a file containing the timing of every phoneme needed to produce the sentence or audio. This first step of conversion can be done with conversion software. An example of such a software is SPRAAK (Demuynck et al., 2008), which is a software that can convert both data types to a segmentation file containing phonemes.

In order to conceptualize this conversion, a graphical representation is shown in Figure 2.11. An audio file is represented which has been segmented in phonemes, along with a segmentation file that has been represented in the graph underneath. Each color is accompanied by a number. Each pair of number and color corresponds with a phoneme. For example, the deep purple (number 42) blocks represent an r, which occurs 4 times in this sequence. Another example is the e, occuring 4 times as well in the sequence, which is represented by the dark orange (number 2) blocks. In the graph, those are the lowest blocks.

Versier de bereiding eventueel met snippers tomaat.



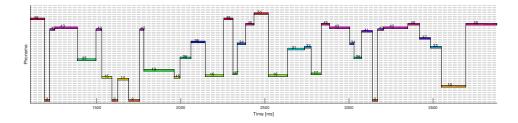
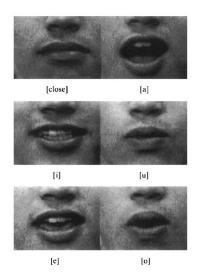


Figure 2.11: A segmented audio file, along with its segmentation file which has been graphically represented underneath, which reads 'Versier de bereiding eventueel met snippers tomaat'.

2.5.2 From phonemes up to visemes

Visemes are a set of mouth patterns that represent the phonemes from before. These set of visemes are predefined and there are not as many visemes as phonemes. As some phonemes like the plosive p and b have a similar shape, they can be represented by the same mouth shape (viseme). An example of a partial viseme set is shown in Figure 2.12a.



(a) Viseme	s, repi	resent	ing <i>a</i> ,	i, u	, e	and	0.
(Hara	& End	do, 20	00)			

No.	Visemes	Phonemes	Example
0	and the same	p,b,m	爸 /bà/
1	and the last	f	发 /fā/
2		t,d, n, m	大/dà/ 毒/dú/ 名/mí ng/
3	-	w	五/wŭ/ 我/wŏ/
4	-	ch,r,sh,zh	沙/shā/ 书 shū/
5		k,g,l, h	歌/gē/ 哈/hō/
6		i	/yī/
7		ai,an	爱/ài/按/àn/
8		a,ang	阿/ā/ 昂/āng/
9		eng,e	饿/è/鞥 (ēng)
10	A 22 PM		

(b) A possible clustering for Chinese Mandarin phonemes, (Qingmei et al., 2008)

In reality, when we speak, the sound as well as the mouth shape used for a certain phoneme is influenced by the prior and subsequent phonemes. This effect has been defined as coarticulation (Ohala, 1993). It is an inertial phenomenon that occurs as the human mouth is not able to accelerate infinitely fast in order to form distinct shapes. Up to today, no known research has taken this effect into account when actuating a robotic mouth.

2.5.3 From visemes up to mouth shapes

Up to today, the conversion step from viseme⁴ up to actuator configuration has always been done manually for a reduced set of visemes (Hara & Endo, 2000; Qingmei et al., 2008; Lin, Cheng, et al., 2011), or has not been mentioned (Lin et al., 2013). This approach is only feasible for a reduced set of mouth shapes. As there is a rich variety of phonemes for any language, it is likely that many of those phonemes have visemes that closely resemble each other. For example the p, b and m. Manual calibration would result in inevitable errors that completely overrule the subtleties of the mouth patterns, which is why clustering is applied (Lin et al., 2013; Qingmei et al., 2008). That is, several phonemes are grouped together and represented by the same viseme. An example of clustering is shown in Figure 2.12b.

2.5.4 From actuator configurations to fluent speech

Using the segmentation file of phonemes and the conversion of those to actuator configurations, one is able to mimic speech in a choppy way. In order to get a more realistic result, a linear interpolation between the central points of the phoneme sequence is carried out (Qingmei et al., 2008).

⁴without taking coarticulation into consideration

Chapter 3

Design of the setup and the mouth

3.1 Introduction

This chapter handles all the parts of designing a setup, which will be used to study the behavior of a prototype mouth. This complete setup has been designed in order to prove that the approach that is proposed in this thesis to calibrate a robotic mouth works. The principles of this approach are explained in Chapter 4.

3.1.1 Preliminary aspects

The design of a mouth has a lot of aspects that have to be taken into account. Some major questions that have to be answered:

- 1. What actuation method will I use?
- 2. How much degrees of freedom do I need?
- 3. How are actuation and mouth connected?

In the literature (see Chapter 2) there are different actuation mechanisms available, all have their advantages and flaws. Seen the advantages of servos and their compactness, servos will be used to actuate the robotic mouth. The questions listed above can be somehow redirected and more precise towards our problem:

- 1. What do I define as a mouth?
- 2. How do I fix a wire to the mouth?
- 3. How many degrees of freedom will I use?
- 4. Will I use the symmetry of the mouth in my advantage?
- 5. How many wires will I therefore use?
- 6. Where are these wires located and what is their direction?

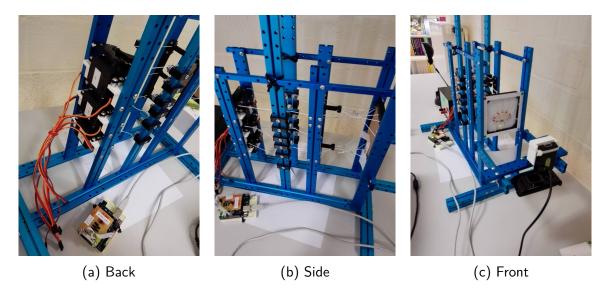


Figure 3.1: The test setup that has been designed during this thesis.

3.2 The test setup

In order to solve those questions, a test setup has been designed (see Figure 3.1). The apparatus uses 5 servo motors to actuate a mouth that is located in a frame, as can be seen in Figure 3.1c. This setup consists of several stages. From the back, a first stage can be found that consists of a rack full of servo motors. From this actuation stage, wires come out and are then pretensioned in the next stage. This stage can change the length of the cable to avoid slack. The next stage is a wireguiding step which guides the wires to the right place. It also fixes the passage of the wire in one spot. In the last stage, wires are guided directly to the mouth through a frame having a set of holes. It is possible to change the direction of the wires in this stage. The wires are at last fed to the mouth where the connection is made with a basic knot. In this setup, there is no space to add a jaw. This is however not a problem as this is not the focus of this thesis.

Using a test setup as this one has the advantage of being modular. Changes can be done relatively fast and experiments can be carried out relatively easy. A camera mount has also been added for this purpose.

3.3 Controlling the setup

3.3.1 Controlling the servo motors

In order to control the servos, the choice has been made to control them directly from Matlab through a Arduino UNO board, as a support package is readily available for that. This means that it is possible to directly control all servos with a simple Matlab command. The power distribution board that feeds the servos is shown in Figure 3.2. On the distribution board, one can notice the presence of a little chip in the center. This chip measures the current drawn



Figure 3.2: The distribution board for feeding the servos

by the servos all together and can be monitored. Doing so, if a blockage of a gear system occurs in any of the servos, the error is immediately seen and the power is shut down to avoid possible damage.

3.3.2 Calibration of the servo motors

The transmission arms connect the servo motors to the wires. These have been designed as such to take as less space as possible. Once these are mounted, a proper calibration is needed. Servo motors are PWM controlled. With the support package, a value between 0 and 1 has to be given which will be mapped between the smallest and biggest (predefined) pulse duration. The servos used have pulse widths between 700 and 2300 μs . Values have been found experimentally to control the servos precisely. They can be precisely controlled between $[-22.5^{\circ}, 22.5^{\circ}]$. This calibration is needed in order keep the servo motors in their safe working range. Doing so, a simplification is made as such that every servo can now be controlled by demanding a simple reference angle.

3.4 Designing the mouth

3.4.1 Preliminary aspects

The design of the mouth is based on a human mouth and thus has an antropomorphic shape. The reason for that is that humans are the only species on earth, capable of mimicing speech, where the mouth has a substantial effect on the understandability of the speaker. If one wants to design a mouth that enhances the understandability of the robot speaking, it thus should have an antropomorphic shape. Next to that, research (Sakamoto et al., 2014) has shown that only the lips and surrounding area contribute to the speech intelligibility when having a

visual perception of the speaker. Taking this in to account, a mouth has been designed, as can be seen in Figure 3.3. As one can see, the mouth has the characteristics of a human mouth and constists only of lips.

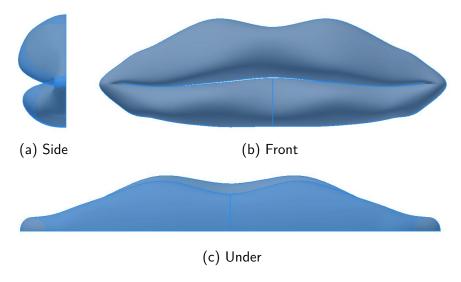


Figure 3.3: The mouth seen from different angles

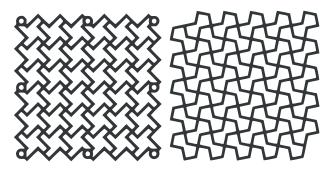
3.4.2 Deformations

The material that has been used for making the mouth is NinjaFlex. It is the market leading flexible filament and it is thus possible to 3D print structures with it. However, it is not extremely stretchy. During a conversation, the mouth deforms, but doesn't stretch much. The only moments when a change of lip circumference is noticable is during protrusion. Protrusion is the phenomena occuring when pouting lips, for example for a kiss, or when expressing the phoneme y (pronouncing as 'oe' in Dutch, 'ou' in French and 'you' in English). In the context of this thesis, pictures of a speaker have been used from prior research (Mattheyses et al., 2011; Mattheyses, 2013). On those pictures, the shape of each phoneme of the Dutch language are shown. Processing those pictures showed that the lip circumference stretches of 23% maximally. This can be attained with Ninjaflex as it can withstand an elongation of 660% according to the manufacturer NinjaTek. For doing so, an internal structure for the lip is needed that can easily deform in order to limit the forces needed.

Internal lip structure

Different planar structures have been studied on deformation. The best one that could be found is the hexagonal structure, as its deformation is more efficient than other structures. Other structures that were tested are shown in Figure 3.4.

A hexagonal structure can deform theoretically in two ways, as shown in Figure 3.5. By theoretically, it is meant without any micro-elongation, only looking at a structure consisting of rigid rods. When we look at the picture, it is clear that the orientation of the hexagon is



(a) A spring structure (b) A spring structure having a 'zigzag' shaped having a 'hourglass' unity cell shaped unity cell

Figure 3.4: Different planar structures that were tested for deformations

important. The first orientation give a poor result: an extension in longitudinal direction of around 15% and a transverse compression of -50%. The second orientation gives a much better result: an extension up to 50% and a compression of -100%. This compression is also seen with a real lip. As the lips are stretched, the lips become thinner, which is what this internal structure allows. In reality, a deformation solely on bending cannot be attended without any stretching, since there is a bending resistance. This bending resistance is defined as follows:

$$R_{bending} = \frac{EI}{L} \tag{3.1}$$

with

- E, the Young modulus;
- I, the area moment of inertia;
- L, the characteristic length of the hexagon.

It is clear that in order to approach the theoretical limit of 50% elongation, \emph{I} has to be as low as possible, meaning that the cross-section of the beam has to be as small as possible, while its length has to be as high as possible. The boundaries of this approach are entirely fixed by the limits of the material and of the 3D printer. For example, the smallest thickness that can be attained is $400\mu m$. The height of a hexagon beam is entirely fixed by the local lip depth.

Another aspect that has to be taken into account is that the lip cannot be a completely closed shell. If this is the case, unnatural warping of the lips will occur. Due to this reason, the lips are left open on top, so that no warping occurs. Taking this into consideration gives the following result as shown in Figure 3.6. The hexagonal structure can be clearly seen.

The internal hexagonal structure has been oriented as such that the deformation of the lips will act as a real lip would behave. That is by looking longer and thinner. Having the hexagonal structure rotated by 30° would not allow that much deformation along the lip circumference, which is now possible.

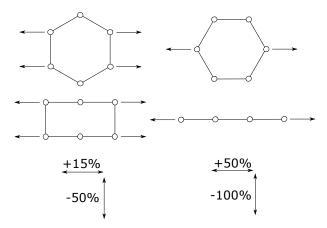


Figure 3.5: The two possible ways to stretch a hexagonal structure.

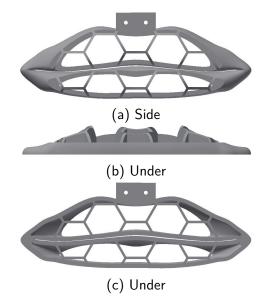


Figure 3.6: The open mouth with a hexagon internal structure, seen from different angles

3.5 Fixation of the wires on the mouth

The connection and positioning of the wires has been established based on the muscular structure around a human mouth (Putz & Pabst, 2009) which is represented in Figure E.1. Its construction is shown in Figure 3.7. As the built frame structure doesn't allow the implementation of a jaw, a push pull system has been constructed with two vertical wires that pull in an antagonistical way. Those two wires represent the effect of the jaw and are actuated with one servo only. As can be seen, only the effect of linear muscles have been taken into account. With this setup, only a pull effect can be applied on the mouth via the wires. The effect of this choice will be shown in chapter 7.

As seen in Figure E.1 in Appendix E, there are several facial muscles that need to be taken

into account. every linear muscle (all but the musculus orbicularis oris, musculus masseter and musculus pterygoideus lateralis) are connected to the musculus orbicularis oris, which surrounds the lips. It is for this reason that the wires have been fixed as close to the border of the lips as possible. The musculus masseter and the musculus pterygoideus lateralis are respectively responsible for the closing of the jaw and protrusion. The latter one has not been implemented due to complexity, meaning that the effect of the musculus pterygoideus lateralis and the musculus orbicularis oris won't be seen: protrusion.

In the designed frame, it is possible to change the direction of the wires as supplementary holes are foreseen.



Figure 3.7: The pose of the wires actuating the flexible mouth. These represent only linear muscles. The represented muscles are shown in Figure E.1 in Appendix E.

Chapter 4

Principle of the method

4.1 Introduction

In this chapter, a new approach will be proposed that allows to actuate any mouth in a fluent way so that it mimics speech, whatever the actuation method behind the mouth and its behavior. In short, the method projects the robots mouth onto a standardised mouth and moves it in such a way that the difference between the two is minimized. Doing this for every basic unit of speech i.e.: for every phoneme, one is able to actuate the robots mouth so that it is able to mimic any speech. This method has been applied to the robotic mouth that has been designed for this thesis. The results are shown in Chapter 7.

4.2 General outline

Let us first recall the general flowchart that has been presented in the literature review 2 of how each approach in the literature handles the calibration of a face robot. The flowchart is shown in Figure 4.1 In here, it is shown that every previous approach but the trial-and-error

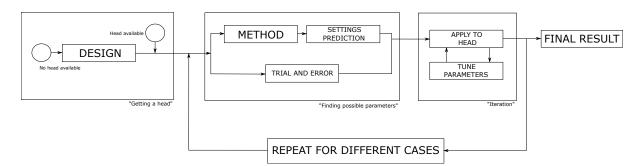


Figure 4.1: A structural graph showing the layout of the applied methods in literature 2.

method did not use the real head when predicting actuator configurations, so the in the end final adjustments have to be carried out.

In Figure 4.2, a flowchart is shown of how this thesis proposes to approach the problem. There is a main difference between the two flowcharts. In the new approach that this thesis

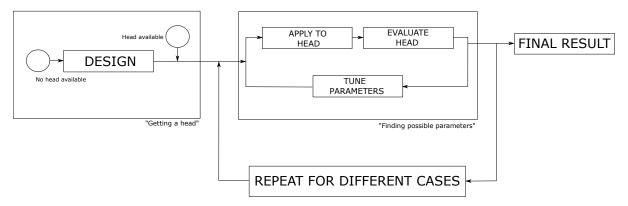


Figure 4.2: A structural graph showing the layout of the new approach proposed in this thesis.

proposes, the actual face robot will be used during the calibration itself. The conversion steps of the new approach are shown in Figure 4.3:

$$\left\{ \begin{array}{l} \mathtt{SENTENCE} \\ \mathtt{AUDIO} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathtt{PHONEME} \\ \mathtt{SEGMENTATION} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathtt{VISEME} \\ \mathtt{SEGMENTATION} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathtt{MOUTH} \\ \mathtt{POSITIONS} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathtt{SERVO} \\ \mathtt{POSITIONS} \end{array} \right\} \vartriangleright \left\{ \begin{array}{l} \mathtt{MOUTH} \\ \mathtt{ACTUATION} \end{array} \right\}$$

Figure 4.3: The different steps up to the actuation of the mouth

The different forms of data in the process are:

- an audio file, a sentence, or any equivalent information form;
- a list of phonemes¹ and an associated segmentation file containing timings;
- a list of visemes² and an associated segmentation file containing timings;
- a set of mouth coordinates, related to previous visemes: The MOUTH POSITIONS;
- actuation parameters that will shape the mouth in question to the desired form;
- a final result matching the desired sentence in a fluent way.

Compared to the forms of data that were shown previously in the literature review (in Section 2.5), there is a difference: between the viseme segmentation and the actual servo positions, there is an extra block: *MOUTH POSITIONS*. This concept will be explained in Section 4.5. Between every information type, is a conversion that has to be done.

¹A phoneme is every basic unit of speech. A language can be represented with a sequence of phonemes.

²A viseme is the visual equivalent of a phoneme.

4.3 From sentence or audio up to phoneme segmentation

The conversion starts with the translation from a sentence or an audio file to a phoneme segmentation file. A phoneme segmentation file is a file containing the timing of every phoneme³ needed to produce the sentence or audio. This first step of conversion can be done with conversion software. An example of such a software is SPRAAK (Demuynck et al., 2008), which is a software that can convert both to a segmentation file with phonemes.

I have had the ability to use audio files that were already converted to phoneme segmentation files. This data is part of previous research (Mattheyses et al., 2011; Mattheyses, 2013). Since the phoneme segmentation files are already available and that this conversion is out of the scope of this thesis, this process won't be detailed. A list of the sentences that are readily available and converted are shown in Table C.1.

In Figure 2.11 on page 14, one of these audio files has been shown, which has been segmented in phonemes, along with that segmentation file that has been represented in the graph underneath. Each number corresponds with a phoneme. The corresponding phonemes are listed in Appendix A. The list of phonemes is complete and can represent the Dutch language completely. It is based on the FONILEX notation (Mertens & Vercammen, 1997), which contains the phonetic transcription of the most frequent word forms of Dutch as spoken in Flanders.

4.4 From phonemes up to visemes

Before being able to convert phonemes to visemes⁴, it is important to clearly define the viseme set. A viseme, being a visual representation of a phoneme, doesn't have a one on one relationship. Several phonemes, like the plosive p and b, do have a similar shape. There are thus not as many visemes as phonemes. The number of visemes can also be more than the number of phonemes, as several phonemes can be mimiced differently. This is due to an inertial effect better known as coarticulation. This phenomenon is what one can remark when uttering different words having the same phonemes. Visemes are altered depending of the phonemes before and after the phoneme in question. In short, a certain phoneme is represented differently, depending on the precedent and subsequent phonemes.

In order to ease the task of linking phonemes to visemes, the pictures that are used have been generated without the effect of coarticulation and are part of previous research (Mattheyses et al., 2011; Mattheyses, 2013). Doing so, every phoneme has a picture representing the mouth shape. Later on, the effect of coarticulation will be brought back in an algebraic way.

Examples of such *viseme representing pictures* are shown in Figure 4.4. The complete set can be found in Appendix B.

 $^{^{3}}$ A phoneme is every basic unit of speech. A language can be represented with a sequence of phonemes. Examples are p, b, m for the Dutch language.

⁴A viseme is the visual equivalent of a phoneme.



Figure 4.4: A subset of *viseme representing pictures*. The complete set that has been used in this thesis can be found in Appendix B.

4.5 From visemes up to mouth positions

Mouth positions are a set of well-defined coordinates (further called POIs, short for Points Of Interest) that are able to represent the shape of the mouth in a compact way. Those have to be generated from a *viseme representing picture*, as well from a picture of the mouth of the robot in question. The choice of those points will greatly influence the resulting mouth positions and thus should be selected with care. In the case of this thesis, cable are actuated through a set of servos that pull the mouth into shape. A good approach in this case consists in selecting the POIs as the fixation points where the cables are attached. This will be favorable in a upcoming step of the algorithm. However, several solutions are possible. More or less POIs can be added. The strength of the method depends on a good choice of POIs. In general, more POIs will result in a better shape. For simplicity, however, it is favorable to have the POIs positioned on the fixation points.

Once the POIs are determined, these have to be normalised in such a way that POIs from a viseme can be compared to the POIs from the mouth of the robot in question. This is necessary, as there is always a scaling mismatch between both mouths. There is only one way in doing that, which is done by only keeping shape information and removing scaling information. For doing this, a reference distance is needed, which is unbiased and not influenced by any shape information. In the case of a mouth, the only reference distance fulfilling these conditions is the lip circumference. This property of the lip is only dependent on the scaling of the lip.

The next step consists in defining an appropriate reference frame. The most straightforward choice, is a reference point which is not moving at all, so that representing movement between several configurations is simplified and clear. There is only one point which can be assumed as non moving, this is the top center point of the lip. This point is shown in Figure 4.5 as well as the reference frame.

When defining the reference frame, it is assumed that the robotic mouth is shown correctly, that is with the lips straight and not tilted compared to the reference frame of the measuring

device (in this thesis, a webcam has been used). If this is the case and this cannot be reduced manually, the measurements of the POI can be used to create a reference frame. In order to do so, the average of each POI is taken as to represent the center of the mouth. The vector formed by this center and the reference POI define the vertical direction, defining a complete reference frame which can be used.

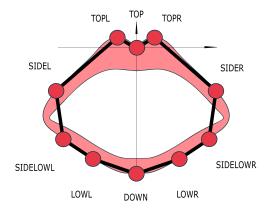


Figure 4.5: The points of interest on a dummy mouth along with the definition of the reference frame of choice.

By now we are able to normalize each POI using the lip circumference, after expressing them in the reference frame of choice.

4.6 From mouth positions up to actuator configurations

Taking the whole system into consideration for the actuation of the mouth can be complicated. Especially non-linearities have to be taken into account if the mouth deforms elastically, as is the case for the mouth that has been designed (see Figure 3.3). What has to be done is find a way to link the behavior of the actuation and the resulting deformations as such, that one finds the necessary configuration of the actuators in order to get the desired deformations. There are several solutions to do that. For example, one could:

- 1. Model the complete behavior of the setup in order to find a link between actuator configuration and desired mouth position;
- 2. Create a database of different actuator configurations in order to look at which configurations give desired mouth shapes;
- 3. Use a feedback algorithm to actuate the mouth.

Modeling the complete behavior of the setup

In order to model the complete behavior of the setup, every single component that has an effect on the system needs to be modeled as well. The most complex part in this thesis is

the mouth itself as it deforms elastically. The mouth has a complex shape which has been designed as such to deform easily. Since it has been designed, CAD models are available. However, there is no information about the manufacturing quality of the mouth itself, which calls for assumptions. The mouth prototype has been 3D printed in a flexible material called *Ninjaflex*. Modeling elastomeric polymers can be done using FEM models but is not simple as big deformations are desired which ensure non-linear elastic behavior.

Creating a database of actuator configurations

In this case, a method is needed to measure deformations quantitatively in a precise way. A solution could be using a webcam along with recognition software, as such that it could determine the position of the mouth in a consistent way.

The method has one big advantage, which is that it omits any need to know the whole behavior of the system in question, as it takes combinations. This method is robust and leads to results. The price to pay is that the method is slow, tideous and cumbersome: First of all, all combinations have to be carried out and pictures have to be taken of the mouth. A lot of them won't be used and are wasted time. Then, recognition software has to loop over all those pictures, finding mouth shape and saving all information necessary. All the pictures that we won't need are evaluated also and will be discarded in the next step. Afterwards, all mouth positions are processed and a link is set between mouth shape and actuator configuration. It is then possible to attribute configurations to all mouth positions who closely fit the reference shapes.

Some questions that have to be asked are the following:

- How much combinations do I need?
- What do I define as 'close enough'?
- What if I am not satisfied with the results?

Those three questions are intertwined: The number of combination depends on how precise you want the result to be, which can be interpreted as what is defined as 'close enough'. Also, stating that you are not satisfied with the results means that the results are not close enough to the reference, which shows that there are not enough combinations close to each other. This little thought experiment reveals that, even being robust, the database has a flaw, which is that you have a contradiction. On the one hand, it is desired to get results close enough, thus needing many combinations, while you do not want many combinations as a lot of them are not used, but still need to be interpreted. These combinations that will not be used take time, which is literally wasted. A partial solute could be to combine several combinations, close to the reference, to form a new set of parameters, which should give closer results. This increases the resolution locally, without increasing the number of combinations drastically, as did the method before. Still, it can be concluded that the method is complex and not optimal.

Use a feedback algorithm to actuate the mouth

The method proposed uses a feedback loop to ensure the closest result possible. Its performance is completely dependent on user defined control.

The concept is the following:

- 1. Set the actuators to a neutral position
- 2. Take a picture of the robotic mouth.
- 3. Recognize the POIs.
- 4. Load the POIs of a standard picture.
- 5. Make sure that the POIs are expressed in the correct reference frames.
- 6. Normalize all POIs with their respective lip circumference.
- 7. Compare both POIs in a non-dimensional space.
- 8. Vectorize the differences of respective POIs.
- 9. Project these vectors in a well-defined way on the actuators line of action.
- 10. Use the signed results as a feedback to the actuation.
- 11. Repeat from step 2 until convergence.

In this thesis, as the POIs are equal to the actuation points, the projection is easy to carry out.

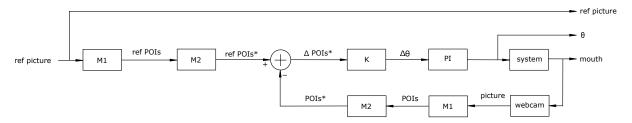


Figure 4.6: The feedback loop of the implemented algorithm. M1 extracts POI data from pictures, while M2 processes those POIs and expresses them in the correct reference frame.

Those steps can be compacted to a control loop as shown in Figure 4.6. In here, the reference picture is compared to the actual mouth position using POIs. The difference is converted into useful values that are then **added** to the actual angles that are requested. This kind of control is an integral control.

Evaluation of the database approach

Preliminary tests have been carried out for the database algorithm. Having 5 servomotors to control, with a working range of 40° , creating a database with a resolution of 5° would take 3 hours to:

- Move servos to the desired position;
- Take a picture;
- Recognize POIs;
- Store angles and POI data.

as the time needed to create the complete data set increases as follows:

$$T_{total} = T_{mean} \prod_{i=1}^{N} \frac{n_i}{\delta_i}$$
 (4.1)

where:

- \bullet T_{mean} is the mean time needed for 1 move only, including all previous steps;
- N is the total number of actuation units;
- n_i is the total working range of actuation unit i;
- δ_i is the resolution used for unit i.

In this case, N=5, $n_i=40$, $\delta_i=5$, gives a total of 59049 combinations. Having $T_{mean}=3$, running the complete database would take 49 hours. In order to put things into context, Table 4.1 shows the time needed for a different amount of servos.

Table 4.1: The time needed to create a database in function of the number of servos. In this case, there are 9 combinations to do for each servo.

n	time	number of combinations
5	49 HOURS	59049
4	5.5 HOURS	6561
3	36 MINUTES	729
2	4 MINUTES	81
1	27 SECONDS	9

It is clear that this solution, while being robust, is not feasible at all for precision and a high number of actuators.

Evaluation of the feedback approach

Regarding the feedback algorithm, tests concluded that the method is robust, but depends on controller gain: This one and only gain is the link between the signed projection of every POI error on a line of action of the actuation and the change of angle that is requested of the actuators.

Changing the gain is influencing the response time of the system, as well as the sensitivity of the system: small errors have a bigger influence when the control gain is important. There is inherently some damping in the system due to friction and others, which keeps the system stable up to some extent. Even if this system discrete, it is perfectly possible to make it instable, which should be avoided at all cost.

The system is assumed to be made out of multiple SISO (Single Input Single Output) systems, while in reality it is a MIMO (Multiple Input Multiple Output) system due to coupling terms generated by the deformable mouth. Every POI has been attributed to a single actuator, thus assuming that and actuator j won't influence a POI i, for $i \neq j$. Due to the inherent construction of the mouth, this influence is not negligible and most importantly in the ability to converge as will be shown next.

High gains result in clearly visible *coupled oscillatory phenomena*, prohibiting the method to converge. Its working principle is simple to understand:

A small error is amplified considerably by a high gain, thus deforming the mouth shape considerably. This action alters the position of an other POI (or more), which on his turn repeats the complete process, resulting in oscillatory movement of the reference angles. An example is shown in Figure 4.7

More than that, there is a treshold present in the servo motors: there is a minimal change of angle needed to affect the position of the servo. This effect amplifies the coupled oscillatory phenomena in such a way that the amplitude of those waves are non-negligible. Their frequency and amplitude mainly depend on the control gain previously defined. The waves shown in Figure 4.7 are not 'classic' system oscillations, which can be seen in the fact that every shock or change in the different actuators happen simultaneously, as well as these waves keep repeating and are not damping out.

Another discontinuity that has to be taken into account is that of the POI detection software. Due to the pixelized image, POI positions are discrete and have integer coordinates before normalizing. This effect introduces microshocks in the system which can further prevent the convergence of the system.

Luckily, this undesired phenoma can be attenuated by using a variable gain technique. Several techniques can give satisfying results. Some of them are shown in Figure 4.8

These techniques vary the control gain in function of the total distance error between all respective POIs. All are reducing the control gain for smaller error, thus having a stabilizing effect on the system dynamics. The most basic technique uses a linear changing gain between $K_{constant}$ and 0.

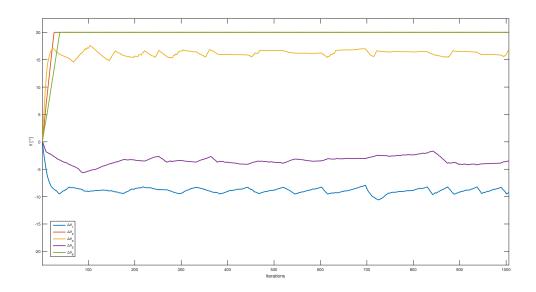


Figure 4.7: The oscillations appearing due to coupling of actuators.

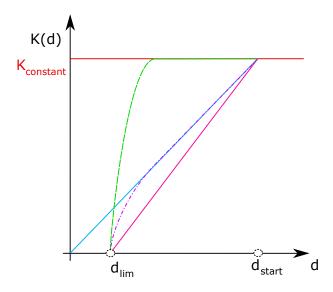


Figure 4.8: Variable gain techniques compared to fixed gain control.

The convergence performance depends greatly on the similarity between the reference and robotic mouths. When big constructional differences exist, there will be a remaining error d_{lim} once the convergence is complete. This d_{lim} cannot be eliminated. This value is mostly depending on the disimilitude of both mouths, but also on the quality of the actuator fixation. If both mouths are similar and POIs are similarly positioned, d_{lim} will be small, while having two different mouths will give a remaining d_{lim} which is not negligible. This will result in a high control gain around convergence, which will still induce coupled oscillations.

A solution for this problem could be to shift the gain between 0 and d_{start} up to d_{lim} and d_{start} , which will greatly reduce this problem. The biggest issue in this case is that d_{lim} is an initially unknown quantity. Since it is mostly dependent on the disimilitude (which is relative) between both mouths, and not on the mouth shapes (which are absolute), d_{lim} will be a relatively constant value for any mouth configuration. This property could be further exploited to predict the value of d_{lim} , in order to fasten the convergence of upcoming calibrations for the next reference mouth shapes. Other variable gain strategies are also shown in Figure 4.8 which further exploit the knowledge of d_{lim} .

In order to emphasize the power of a variable gain strategy, the result of using a linear gain is shown in Figure 4.9. Note that the oscillations are remarquably smaller but still present, since d_{lim} is still non-negligible. In Figure 4.10, a linear gain strategy has been used, which uses a prediction of δ_{lim} to stabilize. As can be seen the convergence is assured. However, its converging speed is lower, compared to the fixed gain strategy shown in Figure 4.7. There, pseudo convergence was attained after 45 iterations, whereas the variable gain strategies need respectively 60 and 120 iterations. These are thus 1.3 and 2.0 times slower. In order to account for this loss, more complex strategies can be used as shown in Figure 4.8.

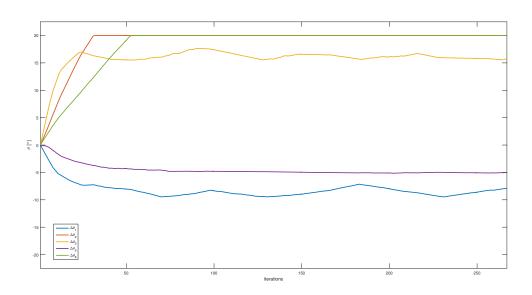


Figure 4.9: Near convergence using a linear varying gain control strategy. The near convergence is due to the dissimilitude between both mouths that is non negligible.

Possible methods to assess d_{lim}

As may have been noticed, it is impossible to know d_{lim} beforehand in order to use a more complex method using the value of d_{lim} . A possible solution for this problem consists in using the d_{lim} of the previous picture and so forth. In order to start, the first picture could be

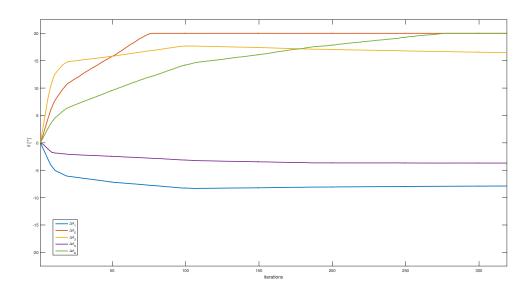


Figure 4.10: The coupled oscillatory phenomena are gone thanks to a variable gain strategy. A linear gain using d_{lim} as origin has been used.

processed omitting the use of d_{lim} and will be refined afterwards using the d_{lim} of the last picture. A question that can be asked is if this iterative change of d_{lim} is really needed as it shouldn't change much of value. Next to that, the calibration of the face robot should be done only once.

Chapter 5

Calibration Software

5.1 Introduction

In order to put the method into practice, software has been created in Matlab. In this chapter, there will be a brief discussion about how the software has been implemented along with some results. First, the recognition software used for converting standard mouth pictures into standard POIs (Points of Interest) is detailed. Secondly, the software used for mapping the servo positions for each standard picture, will be briefly explained.

5.2 Recognition of the POIs for reference mouths

The first important script that has been written is a shape recognition package that allows one to import pictures of mouths and extract mouth shapes. In Figure 5.1, some mouth pictures are shown, that have been used to extract mouth shapes. These pictures are part of previous research (Mattheyses et al., 2011; Mattheyses, 2013). The complete set of them is shown in Appendix B.



Figure 5.1: Some pictures that are used to extract mouth shapes.

These figures have been processed by a Matlab script in order to extract the mouth shape of it. An example of this process is shown in Figure 5.2.

First the original image is cropped in order to contain only the mouth. Next, a transformation is applied in order to remove artificially any effect of shadows. Then, several color mapping are used to increase the difference between the lips and the skin of the subject (upper left image). Then, the *K means* algorithm is applied which groups all pixels that resemble each other together in a predefined number of groups. The result is shown in the lower left image. At last, a new grouping is carried out, separating skin from the rest of the image. The percepted skin is shown in white, whereas the lips are shown in black. The result can be seen in the upper left image.

In order to process this image, the whole dark area is analyzed such as to give a contour. This contour has the shape of the lips we seek. Finally, the POIs that will compact the shape data of the mouth are found by well-defined mathematical conditions that process the complete lip shape. The result is shown in the lower right image.

Applying this strategy for each of the 55 previously defined reference mouths gives us a way to translate rach picture to a set of well-defined POIs.

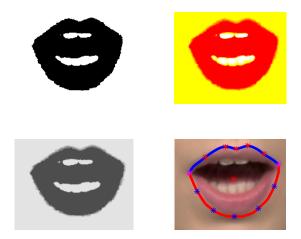


Figure 5.2: The mouth shape recognition script, recognizing the mouth shape (lower right) using a set of color mapping (right up), *K means clustering* (left under) and grouping strategies (left under) in order to find the lip shape. The POIs are found using well defined mathematical conditions.

5.3 Recognition of the POIs for the robotic mouth

In this thesis, a webcam has been used to take pictures of the robotic mouth. The images are analysed in the same fashion as the reference mouth: Distinct POIs are immediately found after pre-processing the images.

5.4 Mapping servo positions with reference shapes

In order to map the previously found POIs of the reference mouth shapes with the POIs of the robotic mouth, software has been implemented that incorporates the principles that were previously defined in Chapter 4. The results are shown in Figure 5.3.

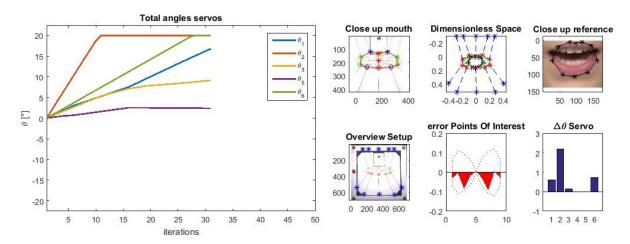


Figure 5.3: The interface of the calibration script that was used throughout this thesis. The interface gives a clear overview of each step during the calibration.

In this picture, several subfigures are shown. The interface gives an *Overview of the Setup* in order to show if the fixation points to the frame are well-defined. This is important as these define the lines of action of each controlled point.

What is also shown a graphical representation of where the POIs of the reference mouths are located (*Close up reference*) as well as those of the robotic mouth (*Close up mouth*). Those two sets are then expressed in the correct reference frame and normalised using the lip circumference (as was explained previously in Section 4.5). Those transformation are then used to combine both results in a *Dimensionless Space*. In this subfigure, the two mouths are represented with their POIs and the line of action of each wire is shown.

The differences of corresponding POIs are vectorized (and shown as green vectors) and projected onto the line of action of each wire. These projections are now signed error measurements which can be used to control the reference position of each servo. These errors are shown in *error Points Of Interest*, for each pair of POIs.

Remark that this result (shown as a red filled area) is symmetric. This is due to the fact that the mouth is actuated symmetrically. This means that several wires are actuated by the same servo. There are in total 9 controllable POIs (along with 1 reference POI that does not move). For those 9 POIs, there are 10 wires, but only 5 servos.

These results are used in concatenated and gained in order to have a meaningfull reference

change for each servo, which is shown in $\Delta\theta$ *Servo*.

After each iteration, these increments are added to the references of each servo, which are then applied for the next iteration. This complete process is repeated until convergence ensues, for each of the 55 pictures. Doing so, the calibration of the robotic mouth is complete. The results are discussed in Chapter 7, whereas the configurations themselve are shown in Appendix D.

Chapter 6

From actuator configurations to actual speech

In the Chapter 4, a method has been given that allows to find an actuator configuration for each mouth standard. In this section, it will be shown how the mouth can be actuated in such a way that it mimics speech in a fluent way.

6.1 Back to basics

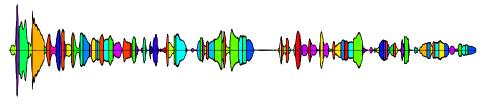
Recalling the general outline of the method (which is shown in Figure 4.3), one could think that having a segmentation file and all actuator configurations for each phoneme, the mouth is only one step away from mimicking speech. This is not the case. There are still some aspects that need to be taken into consideration. In order to make this clear, Figure 6.1 shows what applying a unprocessed segmentation file would give as result:

Sending this data straight to the actuators would give a choppy result, which has to be avoided at all cost. The main goal of this last conversion step is to generate a fluent result. For doing so, different steps will be taken in order to get a convincing result:

- The segmentation will be linearly interpolated in the mid of each segmentation;
- On top of the previous interpolation, parabolic blends are added, representing th effect of coarticulation;
- A clustering of the phonemes will be performed, representing each cluster with a specific representative phoneme;
- Attributing to each phoneme a level of importance, thus excluding those that do not contribute to the understanding of the speech.

The clustering of phonemes and the concept of level of importance will be explained respectively in Sections 6.1.2 and 6.1.3.

Drie dagen voor het begin van de lessen werd ik opgebeld met de mededeling dat de cursus was geannuleerd door een gebrek aan belangstelling.



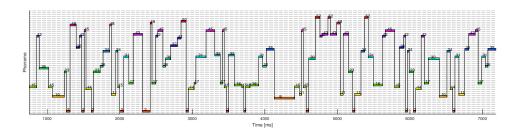


Figure 6.1: A segmented audio file, along with it segmentation file graphically represented underneath, which reads 'Drie dagen voor het begin van de lessen werd ik opgebeld met de mededeling dat de cursus was geannuleerd door een gebrek aan belangstelling'.

6.1.1 Linear interpolation with parabolic blends

As shown in the litterature review (Chapter 2), only linear interpolation has been used to produce continuous speech. In this study, a linear interpolation is used with parabolic blends. The parabolic blends are used to account for the effect of coarticulation, which is an inertial effect that shows the acceleration limits of a real human mouth. Parabolic blends have a constant acceleration. They are thus a good representation of coarticulation.

The implementation that has been used in this thesis is based on literature (Craig, 2004) and uses only one parameter to determine the shape of the parabolic blends. This parameter is the constant acceleration in the blend, $\ddot{\theta}_{max}$.

The maximal acceleration of the actuators can be used as a guideline to fix the value of $\ddot{\theta}_{max}$, if this information is available. If so, this could be used to asses the ability of the servos to keep up with the speech. If an error occurs during the interpolation with $\ddot{\theta}_{max} = \ddot{\theta}_{servos}$, then this means that the selected actuators are not capable to keep up the pace.

There are several solutions for that:

- Use quicker actuators;
- Slow down the speech, while keeping the pitch constant (possible up to -20%);
- Removing phonemes might as well help;
- Replace linear interpolation with parabolic blends by a moving averaging window. This
 will help to some extent.

Quicker actuators cost more and are not the best solution as there are many tricks that can be used to get convincing results with slower actuators. For example, one could slow down the speech. This can be done, while keeping the pitch constant. If not, the speaker will get a lower voice, which has to be avoided. Solutions for this problem exist and there are several implementations available to slow down speech while maintaining a constant pitch. The function that has been used for this purpose has been implemented by (Ellis, 2002), which is an implementation of the Phase Vocoder algorithm (Flanagan & Golden, 1966).

6.1.2 Clustering phonemes

Clustering phonemes is used in a lot of applications. The main reason for using clusters is to avoid over-articulation, which would result in exaggerated mouth poses. A set of phonemes representing the basic units of a language, often have a lot of similarities, regarding shape and type. For example, the plosive p and p have a similar shape (as seen in Figure 6.2), although the location of the sound formation in the mouth is different.

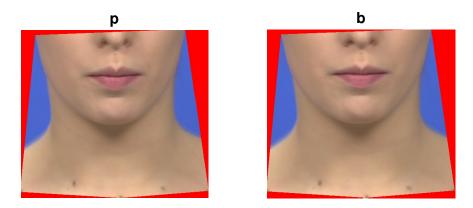


Figure 6.2: The similar visual representations of phonemes p and b

Clustering groups have been defined for Dutch in literature (van Son, 1994). This listing has been completed with extra notations that are typical for the YAPA notation, as this notation has been used for the segmentation files of (Mattheyses et al., 2011; Mattheyses, 2013). The YAPA notation is a notation that has been defined as such to write down phonemes with ASCII characters, in order to implement computer algorithms in a simpler way. The list of clusters is shown in Table 6.1. 11 groups have been defined and each of them is represented by a specific viseme. For example, the f, v and w have been clustered and will be represented by the viseme for w.

6.1.3 Phoneme importance levels

During a conversation, people may find the necessity to enhance understandability of the counter player. They can improve that by lip reading the speaker. During lip reading, one

¹ A plosive is a consonant in which the vocal tract is blocked so that all airflow ceases. Examples of plosives are k, g, p, t, b and d.

Table 6.1: The clustering of phonemes that has been used, is based on (van Son, 1994) and has been augmented with phonemes (which are <u>underlined</u>) that are specific for the YAPA notation.

cluster_number	members	representative	
1	b, p, m, mcap	Ь	
2	f, v, w	W	
3	s, scap, z, zcap	S	
4	d, j, jcap, l, n, t	t	
5	g, gcap, h, k, ncap, r, x	k	
6	\mathcal{O} , $E\sim$, e, emarg, i, icap, emargj, ecap, <u>ieuw</u> , <u>eeuw</u> , aj	e	
7	A∼, a, acap	а	
8	@marg, $O\sim$, $Y\sim$, ocap, u, y, ycap, oj, <u>oei</u> , <u>uw</u>	ycap	
9	ampers, o, omarg	0	
10	9, @marg9, omargw	@marg9	
11	_	_	

seeks for characteristic visemes which indicate possible phonemes (for example as in Figure 6.2), that can be grouped to possible words. During this decryption, some phonemes are more valuable for deciphering mouth shapes to speech. The reason for that is because of coarticulation. Some phonemes are considerably more coarticulated than others, making them **invisible**. Other phonemes are kept intact, which will be called **protected**. Off course there is a transition between these two groups, where phonemes suffer less deformation but which is not negligible. Those phonemes are **normal**. In Appendix C, a list of phonemes has been enriched with levels of importance. In this list, invisible phonemes are tagged as **INV**, normal phonemes as **MID** whereas protected phonemes are named **PTD**. The proportion of each group is shown in Table 6.2.

Table 6.2: The presence rate of each phoneme group

	PTD	MID	INV
presence rate [%]	34.5	47.3	18.2

In order to increase the understandability of the robotic mouth, invisible phonemes will be left out intentionally, giving more 'time' for protected phonemes, enhancing the speech quality. This is not real time that is given but more place (in the time domain) to smooth out with coarticulation. Besides, possible calibration errors on invisible phonemes will not be shown which is an other advantage. The effect of hiding the invisible phonemes is shown in Figure 6.3. In the graph above, linear interpolation is applied, while in the lower graph, parabolic blends are added, showing that hiding invisible phonemes gives more 'time' for coarticulation. The mean distance between points in the interpolations is longer, while the position of the phonemes remains unchanged.

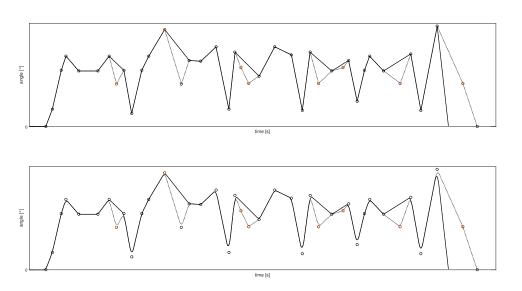


Figure 6.3: The influence of hiding invisible phonemes in the segmentation file. In the graph above, linear interpolation is applied, while in the lower graph, parabolic blends are added, showing that hiding invisible phonemes gives more 'time' for coarticulation.

Chapter 7

Tests and results on the setup

7.1 Introduction

In this Chapter, the results of the tests that have been carried out on the setup are out are shown. First, the calibration results are shown compared to the reference pictures.

7.2 Calibration of the test setup

One calibration of the setup has been carried out. The calibration has been done for 55 reference mouth shapes, that were previously defined by (Mattheyses et al., 2011; Mattheyses, 2013). These 55 reference mouth shapes represent each of the 55 phonemes defined by the FONILEX manual (Mertens & Vercammen, 1997). As explained previously in Section 6.1.2, a clustering has been carried out, meaning that several phonemes are visually represented by the same picture. Since 55 pictures are a lot, only the results for each cluster are shown.

In Figures 7.1 and 7.2, the mouths representing each cluster are shown, along with the reference picture. There has been no tuning of the parameters after the calibration has been carried out. These are raw results. The angular configuration of each servo has been listed for each of the 55 pictures in Appendix ??.

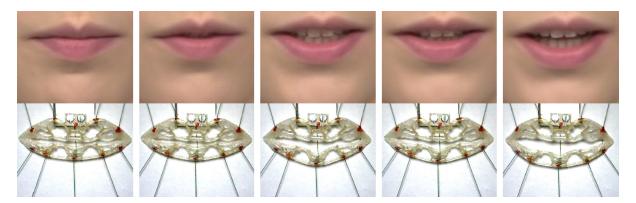


Figure 7.1: The calibration results compared with the reference mouths for the first 5 out of 11 clusters. The pictures represent each cluster and correspond respectively with b, w, s, t and k.

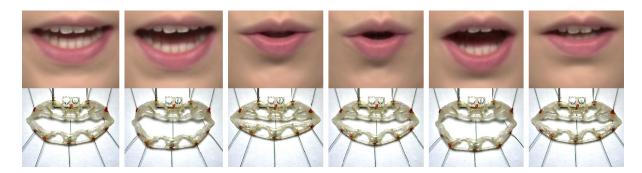


Figure 7.2: The calibration results compared with the reference mouths for the last 6 out of 11 clusters. The pictures represent each cluster and correspond respectively with e,a,ycap,o, @marg9 and _.

Figures 7.1 and 7.2 prove that the new method works. It is possible to calibrate the mouth setup with several reference pictures, which gives very convincing results. There are however several differences that can be seen in the results:

- 1. Protrusion cannot be shown, which means that *y* (pronounced as 'oe' in Dutch and 'u' in English), will have a biased result. This can be seen in Figure 7.2 in the third and fourth picture from the left. This is due to the fact that the lip length of the mouth setup cannot be controlled, since the M. orbicularis oris has not been implemented. This error is not due to the method.
- 2. No push-pull cables were used. Due to this, there is a possible saturation that has occured in the control, which can be seen in the angular servo settings in appendix $\ref{eq:consistent}$??. The results are represented graphically in Figure 7.3 Some values of the servos are consistently on the limits of each servo (that have been set to -20° and 20° for safety reasons). This is due to two reasons: on the one hand, pushing is not possible, so that the controlled system will try to push further until angle saturation occurs. This effect can be seen visually if there is slack in the cables. On the other hand, this saturation

- could also occur if the required angular positions are outside the working range of the system, meaning that the system is badly designed. It has been verified that each saturating servo had slack in the cable.
- 3. The POIs were defined on the outer side of the lips. Due to this choice, it is possible to have a mouth that is nearly closed, while the reference is completely closed. In order to solve this problem, POIs could be defined on the inner part of the lips, in order to make sure that the lips will not be apart when they are supposed to be closed. The parting level of the lips when completely closing is desired depends on the dissimilitude of both mouths regarding lip thickness.

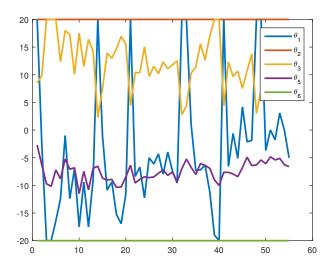


Figure 7.3: The calibration results, graphically represented for each of the 55 mouth shapes. Some values of the servos are consistently on the limits of each servo (that have been set to -20° and 20° for safety reasons). This is due to two reasons: on the one hand, pushing is not possible, so that the controlled system will try to push further until angle saturation occurs. This effect can be seen visually if there is slack in the cables. On the other hand, this saturation could also occur if the required angular positions are outside the working range of the system, meaning that the system is badly designed. It has been verified that each saturating servo had slack in the cable during saturation.

Chapter 8

Conclusions

8.1 Fullfilment of the goals

The results with the robotic mouth that have been detailed in Chapter 7 show promising results. The goals of this thesis that were previously defined were:

The goal of this thesis is to present a new approach that could be used to calibrate robotic mouths in order to properly mimic speech.

In order to validate this concept, a test setup has to be designed, consisting of a robotic mouth, which will be calibrated with the new approach.

The quality of the approach will be assested by the use of a lip-synchronisation module, which will allow to mimic speech.

The new approach should be able to:

- 1. Calibrate the robotic mouth by omitting the complete knowledge of the robotic head;
- 2. Do this fully automatically;
- 3. allow an objective evaluation about the configuration quality of the DOFs that are implemented in the mouth.

In this thesis, a test setup has been proposed, having a robotic mouth. A new approach has been proposed to calibrate the robotic mouth automatically, without any knowledge of the complete system. In Chapter 7, it has been shown that the results given by the method allow to evaluate the configuration of degrees of freedom objectively. Also, these results have shown that the calibration gives convincing results.

No text to speech module results have been shown. These results will be presented on this thesis' defence by showing several videos.

8.2 Discussion

The method that has been proposed has used the projection of the robotic mouth onto planar reference mouth shapes. However, the method is not constrained to the use of planar references. For example the use to 3D scanning adevices (as for example provided by Vixon, leader in this technology), can give 3D data of how an animatronic head would look like. The same can be done with reference data, coming from a real person that has been scanned as well. The main difficulty here would be to shape these two data sets as such that they can be compared. In other words, the main difficulty would be to project the two faces onto a reference head that is standardised.

This standardisation has been carried out as well by using the lip circumference of the lips to allow a comparison between robotic mouth shapes and reference mouth shapes.

This means that the approach proposed in the thesis could be used to calibrate complete animatronic heads, not only for mimicing speech, but also to express emotions.

8.3 Future work

The proposed approach is very general and has been implemented in order to calibrate animatronic mouths, using planar projections. Future research could be conducted on how this approach can be used to project complete faces to a standardised shape, in order to be to compare complete face forms. In this context, it would be interesting to study the calibration quality of this approach and to see if it can be used to control any animatronic head.

Appendices

Appendix A

List of all phonemes for Dutch

In this part of the appendix, one can find a list of all phonemes for the Dutch language. These are represented in Figure A.1. These are shown in different notations, *YAPA-FONILEX-BROAD*, *YAPA-FONILEX-BROAD* and *IPA*. Next to that, examples of use are shown, along with the level of importance of each phoneme, as defined in Section 6.1.3.

The list of phonemes is complete and can represent the Dutch language completely. It is based on the FONILEX notation (Mertens & Vercammen, 1997), which contains the phonetic transcription of the most frequent word forms of Dutch as spoken in Flanders.

N.	YAPA-FONILEX-BROAD	YAPA-FONILEX- BROAD	IPA	Example	Lol
1	9	9	Ч	int <u>uï</u> tief	MID
2	@	@	ə	d <u>e</u>	MID
3	@marg	@:	œ	fr <u>eu</u> le, <u>oeu</u> vre	MID
4	@marg9	@:9	œY	h <u>ui</u> s	MID
5	A~	A~	đ~	croissant	MID
6	E~	E~	٤~	vacc <u>in</u>	MID
7	0~	0~	o~	c <u>o</u> ngé	MID
8	Y~	Y~	γ~	parf <u>um</u>	MID
9				empty	MID
10	<u>-</u> а	<u>–</u> а	a a	n <u>aa</u> m	PTD
11	acap	A	a	p <u>a</u> t	MID
12	aj	aj	-	dr <u>aai</u>	PTD
13	ampers	&	ø	d <u>eu</u> r	MID
14	b	b	b	<u>b</u> ak	PTD
15	d d	d	d	<u>d</u> ak	INV
16	e	e	e	v <u>ee</u> r	PTD
17	ecap	E	8	p <u>e</u> t	MID
18	emarg	E:	8	cr <u>è</u> me, milit <u>air</u>	MID
19	emargj	E:j	21	f <u>i</u> in	MID
20	ew	ew	Ci	sn <u>eeuw</u>	PTD
21	f	f	f	<u>f</u> el	PTD
22				goal, za <u>k</u> doek	INV
23	g	g G	g Y		
24	gcap h	h	h	goed, zegen	INV
25	i			<u>h</u> and	INV
26		i I	i I	v <u>ie</u> r	PTD
27	icap			p <u>i</u> t	MID
28	iw :	iw :		n <u>ieuw</u> :-	MID
28 29	j !	j	j	<u>j</u> a	INV
	jcap '	J	'n	ora <u>nj</u> e, champa <u>gn</u> e	INV
30	k	k	k	<u>k</u> ap	INV
31	I	I	I	<u>l</u> and	MID
32	m	m	m	<u>m</u> et	PTD
33	mcap	М	m	ka <u>m</u> fer, aa <u>n</u> valt	PTD
34	n	n	n	<u>n</u> et	INV
35	ncap	N	η	ba <u>ng</u>	MID
36	О	0	0	v <u>oo</u> r	PTD
37	ocap	0	Э	p <u>o</u> t	MID
38	oj	oj		m <u>ooi</u>	PTD
39	omarg	O:	Э	r <u>o</u> ze, z <u>o</u> ne	MID
40	omargw	O:w	ЭÜ	<u>gou</u> d	PTD
41	р	р	р	<u>p</u> ak	PTD
42	r	r	r	<u>r</u> and	MID
43	S	S	S	<u>s</u> ein	MID
44	scap	S	ſ	<u>sh</u> ow, <u>si</u> aal	MID
45	t	t	t	<u>t</u> ak	INV
46	u	u	u	r <u>oe</u> r	PTD
47	uj	uj		r <u>oei</u>	PTD
48	V	V	V	<u>v</u> el	PTD
49	w	w	W	<u>w</u> it	PTD
50	x	x	х	to <u>ch</u>	INV
51	У	У	У	v <u>uu</u> r	PTD
52	ycap	Υ	Υ	p <u>u</u> t	MID
53	yw	yw		d <u>uw</u>	PTD
54	z	Z	Z	<u>z</u> ijn	MID
55	zcap	Z	3	baga <u>g</u> e	MID

Lol = Level of Importance

Figure A.1: All the phonemes for the Dutch language in different notations, along with examples of their use and their level of importance.

Appendix B

Complete viseme set

In this part of the appendix, a list is given were each phoneme is represented by a different viseme, in Figure B.1. The effect of coarticulation has been iteratively removed by combining different appearances of the same phoneme. This is why in some pictures a second row of teeth seems to appear. This data comes from (Mattheyses et al., 2011; Mattheyses, 2013).



Figure B.1: The visemes that are allocated to each phoneme for the Dutch language.

Appendix C

Default sentences

In this part of the appendix, a list is given with each of the default sentences available from (Mattheyses et al., 2011; Mattheyses, 2013), along with a translation to English.

Table C.1: Standard sentences in Dutch along with their translation in English

Number	Language	Sentence
1	NL EN	Versier de bereiding eventueel met snippers tomaat. You can eventually finish the preparation with snippets of tomato.
2	NL EN	In het verslag analyseer je wat er fout gegaan is. Analyze the mistakes in the report.
	NL	Er loopt nog steeds veel politie op straat en er rijden nog steeds wagens met veel militairen rond.
3	EN	There are still a lot of policemen on the street and military trucks driving.
	NL	Drie dagen voor het begin van de lessen werd ik opgebeld met de mededeling
4	EN	dat de cursus was geannuleerd door een gebrek aan belangstelling. I was called three days before the first lesson with the notification that the course was cancelled due to a lack of interest.
5	NL EN	De groene partij moet daarbij een aantal harde noten kraken. The green party has to crack some tough nuts.
6	NL EN	In het stuk is zijn favoriete vergelijking die van de mens als messentrekker. His favorite comparison in the play is that of the man as stabber.
	NL	Vaak zelfs de ziel van mensen om wie je het meeste geeft, in wie je veel van
7	EN	je energie, geduld en liefde gestoken hebt. Often even the soul of people who you care most about, whom you gave a lot of energy, patience and love.
8	NL EN	Vandaar dat de sector het medium frequent gebruikt. Which is why this medium is often used by this sector.
	NL	De firma's oordelen dat de verkoop van hun producten daardoor nadelig
9	EN	beïnvloed kan worden. The companies estimate that the sales of their products can be badly influenced.
10	NL EN	De dertien slachtoffers van het militaire geweld zijn vandaag begraven. The thirteen victims of military aggression were buried today.

Appendix D

Servo calibrations

In this part of the appendix, the calibration results of the setup are shown. These were generated with the new approach presented in this thesis, with no tuning at all in the final results.

Table D.1: The calibration values of each servo for the mouth positions from 1 up to 25. These values were generated completely autonomously by the algorithm.

N.	$ heta_1[^\circ]$	$\theta_2 [^\circ]$	$\theta_3[^\circ]$	$\theta_5 [^{\circ}]$	$\theta_6 [^{\circ}]$
1	20.00	20.00	8.54	-2.71	20.00
2	-2.71	20.00	9.81	-6.35	20.00
3	-20.00	20.00	20.00	-9.72	20.00
4	-20.00	20.00	20.00	-10.17	20.00
5	-16.43	20.00	20.00	-7.21	20.00
6	-12.41	20.00	12.36	-8.81	20.00
7	-0.99	20.00	18.00	-5.24	20.00
8	-12.39	20.00	17.23	-7.08	20.00
9	-7.01	20.00	10.10	-6.82	20.00
10	-17.47	20.00	17.52	-11.49	20.00
11	-9.43	20.00	11.53	-7.47	20.00
12	-17.51	20.00	16.40	-10.81	20.00
13	-8.90	20.00	14.21	-6.90	20.00
14	20.00	20.00	2.27	-6.54	20.00
15	-1.00	20.00	7.43	-8.70	20.00
16	-10.85	20.00	13.91	-9.01	20.00
17	-9.39	20.00	12.98	-8.93	20.00
18	-15.28	20.00	14.71	-10.37	20.00
19	-16.93	20.00	16.93	-10.29	20.00
20	-11.58	20.00	15.54	-8.51	20.00
21	20.00	20.00	4.42	-6.37	20.00
22	-8.39	20.00	10.38	-9.57	20.00
23	-6.71	20.00	10.38	-8.93	20.00
24	-12.26	20.00	15.03	-8.46	20.00
25	-5.01	20.00	9.70	-8.61	20.00

Table D.2: The calibration values of each servo for the mouth positions from 26 up to 55. These values were generated completely autonomously by the algorithm.

N.	$ heta_1[^\circ]$	$ heta_2[^\circ]$	$\theta_3[^\circ]$	$ heta_5 [^\circ]$	$ heta_6 [^\circ]$
26	-6.13	20.00	11.54	-8.48	20.00
27	-4.32	20.00	10.21	-7.80	20.00
28	-7.98	20.00	12.35	-7.21	20.00
29	-3.98	20.00	11.07	-8.19	20.00
30	-7.42	20.00	11.79	-7.59	20.00
31	-9.58	20.00	12.51	-9.38	20.00
32	20.00	20.00	2.81	-7.01	20.00
33	20.00	20.00	4.35	-5.24	20.00
34	1.07	20.00	10.30	-6.74	20.00
35	-7.29	20.00	11.39	-8.02	20.00
36	-7.20	20.00	15.60	-6.07	20.00
37	-6.34	20.00	12.68	-6.39	20.00
38	-11.18	20.00	16.98	-6.92	20.00
39	-19.01	20.00	20.00	-9.00	20.00
40	-20.00	20.00	20.00	-10.02	20.00
41	20.00	20.00	4.41	-7.64	20.00
42	-6.54	20.00	12.29	-7.65	20.00
43	-0.62	20.00	9.69	-7.95	20.00
44	-5.10	20.00	10.66	-8.43	20.00
45	4.19	20.00	7.54	-6.80	20.00
46	-2.13	20.00	10.73	-4.89	20.00
47	-1.87	20.00	13.75	-6.42	20.00
48	20.00	20.00	3.03	-6.31	20.00
49	20.00	20.00	7.25	-5.41	20.00
50	-3.69	20.00	9.70	-6.11	20.00
51	0.02	20.00	8.79	-4.83	20.00
52	-1.76	20.00	9.71	-5.40	20.00
53	3.08	20.00	9.46	-5.12	20.00
54	-0.06	20.00	8.83	-6.28	20.00
55	-5.01	20.00	11.26	-6.60	20.00

Appendix E

Anatomy of a human face

In this part of the appendix, the primary muscles that have a direct effect on the deformation of the lips are shown.

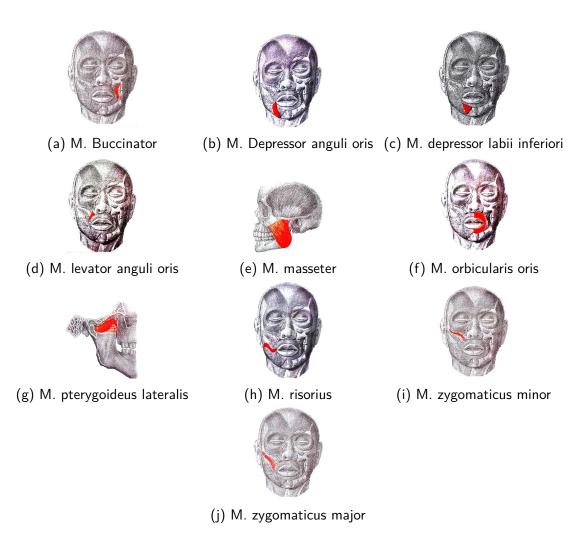


Figure E.1: The major muscles having a direct effect on the deformation of the lips. (Putz & Pabst, 2009)

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